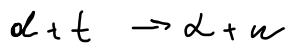


$\langle \sigma v \rangle$: reactivity

$$\frac{\text{# reactions}}{\text{time volume}} = \langle \sigma v \rangle \cdot n_d n_t$$



50:50 DT mixture

$$n_d + n_t = n_e \Rightarrow n_d = n_t = \frac{n_e}{2}$$

$$\frac{\text{# reactions}}{\text{time volume}} = n_e^2 \frac{\langle \sigma v \rangle}{4}$$

Scion / Heating



S_α

2) Auxiliary heating

S_h

Cooling

- 1) Emission of radiation (Bremsstrahlung)
- 2) Transport of heat

S_K

S_B

S_α : E_α : en. released by α s in each fusion reaction
 $E_\alpha \approx 3.5 \text{ MeV}$

$$S_\alpha = E_\alpha \cdot \left(\frac{\# \text{reactions}}{\text{volume time}} \right) = E_\alpha \frac{n_e^2}{4} \langle \sigma v \rangle$$

$$P = n T$$

$$P_{T\sigma} = P_e + P_\alpha + P_t = \underbrace{n_e T}_{\frac{n_e}{2}} + \underbrace{n_\alpha T}_{\frac{n_e}{2}} + \underbrace{n_t T}_{\frac{n_e}{2}} = \frac{2n_e T}{2} \Rightarrow n_e = \frac{P}{2 T}$$

$$S_\alpha = E_\alpha \frac{P^2}{16T^2} \langle \sigma v \rangle$$

S_h :

$$S_B = C_B \cdot \underbrace{z_{eff}}_1 n^2 \cdot T^{\frac{1}{2}} = \frac{1}{4} \cdot C_B \frac{P^2}{T^{\frac{3}{2}}}$$

$n = \frac{P}{2T}$

$$S_K = \frac{3}{2} \frac{P}{\tau_E} \quad \tau_E: \text{energy confinement time}$$

$$P \ T \ \tau_E$$

Practical units

$$S_\alpha = k_\alpha \frac{P^2}{T^2} \frac{MW}{m^3} \quad k_\alpha = 1.37$$

$[T] = keV$

$[P] = bAr$

$[S_E] = 10^{-22} m^2/s$

$$S_B = k_B \frac{P^2}{T^{\frac{3}{2}}} \frac{m w}{m^3} \quad k_B = 0,052$$

$$S_K = k_K \frac{P}{T_E} \frac{m w}{m^3} \quad k_K = 0,15$$

Power balance:

$$\text{heating} = \text{cooling}$$

$$S_H + S_\alpha = S_K + S_B$$

1) Ideal ignition

$$\begin{array}{ccc} \xrightarrow{\quad} & \xrightarrow{\text{Ideal}} & \xrightarrow{\quad} \\ S_H = 0 & S_K = 0 & \text{ignition} \\ S_\alpha \geq S_B & & \end{array}$$

$$k_K \frac{(T)}{T^{\frac{1}{2}}} \cancel{k_B} \geq k_B \cancel{P} \cancel{T^{\frac{3}{2}}} \cancel{k_B}$$

$$\frac{\langle \sigma v \rangle(T)}{T^{\frac{1}{2}}} \geq \frac{k_B}{k_K}$$

$$T_{\min} = 1.1 \text{ keV}$$

2) Ignition

$$S_d \geq S_B + S_K \quad (\delta_h = 0)$$

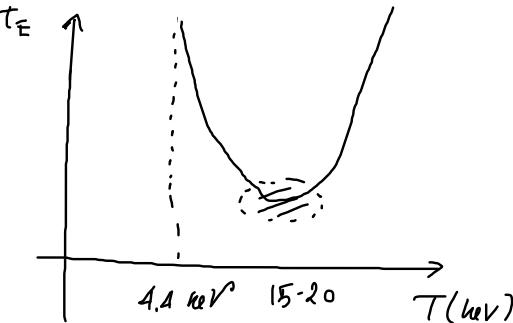
$$P^T T_E \quad k_d \frac{\langle \sigma v \rangle}{T^2} P \geq \frac{k_B P}{T_E^{3/2}} + k_n P$$

$$P T_E \geq \frac{k_n T^2}{k_d \langle \sigma v \rangle - k_B T^{1/2}}$$

Minimum

$$T_{\min} = 1.1 \text{ keV}$$

$$(P T_E) = 8 \text{ atm} \cdot \text{s}$$



$$p = 2nT$$

$$p\tau_E T = 8 \text{ atoms} \cdot s \cdot 15 \text{ keV}$$

$$2nT\tau_E T = 8 \text{ atoms} \cdot s \cdot 15 \text{ keV}$$

$$n\tau_E T = \frac{8 \text{ atoms} \cdot s \cdot 15 \text{ keV}}{2 \cdot 15 \text{ keV}} = \dots \approx 3 \cdot 10^{21} \text{ keV m}^{-3} \cdot s$$

dawson criterion

$$T \approx 15 \text{ keV}$$
$$n \approx 10^{20} \text{ m}^{-3} \quad \tau_E \approx 5$$

if

$$s_h \neq 0$$

$$f_\alpha = \frac{s_\alpha}{s_\alpha + s_h}$$

$$\text{if } s_h = 0 \quad f_\alpha = 1 \quad (\text{ignition})$$

$$\text{if } f_\alpha \geq \frac{1}{2}$$

ITER

$$\text{if } s_h = s_\alpha \quad c_\alpha^P = \frac{1}{2}$$

$$S_h = \frac{1 - f_\alpha}{f_\alpha} \cdot S_{av}$$

$$S_d + S_h \geq S_k + S_B$$

$$S_d + \frac{1 - f_\alpha}{f_\alpha} S_{av} \geq S_k + S_B$$

$$\frac{S_d}{f_\alpha} \geq S_k + S_B; \quad S_{av} \geq f_\alpha (S_k + S_B)$$

$$P\tau_E \geq \frac{P}{f_\alpha} \cdot (P\tau_E)_I$$

$$Q = \frac{\text{net thermal power}}{\text{total input power}} = \frac{P_{out} - P_{in}}{P_{in}} \quad Q = 1 \text{ breakeven}$$

$Q = \infty$ ignition

Factors that contribute to power out:

1) Bremsstrahlung

Cannot use: S_{α}

2) neutrinos

3) Heat due to transport

$$Q = \frac{P_{out}}{P_{in}} = \frac{\overbrace{4S_{\alpha} + S_B + S_K - S_H}^{\text{neutrinos}}}{S_H} = \frac{\cancel{S_H}}{\cancel{S_H}} \frac{5S_{\alpha}}{S_H} = \frac{P_{fusion}}{P_{heating}}$$

$$\frac{S_K + S_B - S_{\alpha}}{S_K + S_B - S_{\alpha}}$$

$$Q = \frac{\frac{5\rho T_E}{k_u T^2} - k_u \langle \sigma v \rangle P_E}{\langle \sigma v \rangle P_E} = \frac{\frac{5\rho T_E}{(\rho T_E)_{\text{ignition}} - \rho T_E}}{(\rho T_E)_{\text{ignition}} - \rho T_E}$$

at ignition: $\rho T_E = (\rho T_E)_{\text{ignition}}$

$$Q = +\infty$$

If not at ignition: $\rho_{T_E} = f_{\alpha} (\rho_{T_E})_I$

$$\frac{Q}{f_{\alpha}} = \frac{5 f_{\alpha} (\rho_{T_E})_I}{(\rho_{T_E})_I - f_{\alpha} (\rho_{T_E})_I} = \frac{5 f_{\alpha}}{1 - f_{\alpha}}$$

$$f_{\alpha} = \frac{Q}{Q + 5} \quad \text{jet} \quad \frac{Q}{f_{\alpha}} = 0.65$$

ρ_T

(1997: transient)

$f_{\alpha} \approx 12\%$

16 MW fusion power
 $\approx 100 \text{ ms}$

Divertor tokamak test

$$\rho_E = \frac{\text{Electrical power}}{\text{Heating power}} \approx 40 \quad \text{ITER}$$

ITER

$\rho = 10$ $f_{\alpha} = 67\%$

Start in

≈ 2027

$\rho_E \approx 10$